

►设计计算◀

往复泵偏置式曲柄滑块机构的运动和动力分析

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摘要 为了了解偏置结构的性能特点和提高往复泵的设计水平,探讨了偏置对曲柄滑块机构的运动和动力的影响。阐述了偏置式和对心式2种结构的基本特点,通过图解和计算分析了偏置对冲程长度、柱塞吸入和排出速度、连杆传力性能及十字头对导板正压力的影响,得出正偏置可以提高连杆传力性能,降低十字头对导板正压力的结论。采用正偏置结构设计的SPM TWS600S型柱塞泵在油田使用效果很好。

关键词 往复泵 偏置 曲柄滑块机构 运动分析

油田使用的压裂泵、固井泵和钻井泵几乎都是往复泵,而往复泵的动力端系统实际上就是多个曲柄滑块机构,十字头就是滑块。曲柄滑块机构有对心式和偏置式之分。所谓对心式,指滑块的运动迹线通过曲柄的旋转中心,偏置式指滑块的运动迹线与曲柄的旋转中心有偏置距 e 。探讨偏置对曲柄滑块机构的运动和动力的影响,了解偏置结构的性能特点,对于偏置结构的应用及往复泵设计水平的提高有实际意义。

运动和动力分析

偏置有正偏置和反偏置,对于动力往复泵来讲,若曲柄在前极限位置时的转向与偏置距 e 离开 OX 轴的方向相反(如图1),则称十字头为正偏置,若曲柄在前极限位置时的转向与偏置距 e 离开 OX 轴的方向相同,称十字头为反偏置^[1]。

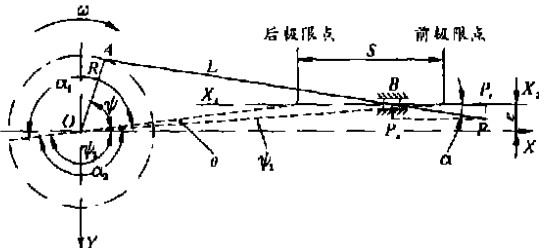


图1 正偏置曲柄滑块机构

下面,笔者分析十字头正偏置时对冲程 S 、柱塞速度 v 以及连杆传力性能的影响。

定义连杆长度为 L (m),曲柄半径为 R (m),连杆比 $\lambda = R/L$,偏置比 $\epsilon = e/R$,曲柄转速为 ω (rad/s),转向如图1所示。曲柄转角为 α (rad),其值在 $(-\pi, \pi)$ 之间变化。曲柄 OA 在 OX 轴上方时, α 为负值(如图1所示);曲柄 OA 与正向的 OX 轴重合时, $\alpha = 0$;曲柄 OA 在 OX 轴下方时, α 为正值。令柱塞在前后极限位置时曲柄转角分别为 α_1 (rad)、 α_2 (rad),令极位夹角为 ψ (rad),令排出和吸入冲程时曲柄转角范围分别为 α_1 (rad)、 α_2 (rad),则有

$$\alpha_1 = -\arcsin \frac{e}{L+R} = -\arcsin \frac{\epsilon}{1+\lambda} \quad (1)$$

$$\alpha_2 = \arcsin \frac{e}{L-R} = \arcsin \frac{\epsilon}{1-\lambda} \quad (2)$$

$$\psi = (\alpha_2 - \alpha_1) = \arcsin \frac{\epsilon}{1-\lambda} - \arcsin \frac{\epsilon}{1+\lambda} \quad (3)$$

$$\alpha_1 = -\arcsin \frac{\epsilon}{1+\lambda} \quad (4)$$

$$\alpha_2 = \arcsin \frac{\epsilon}{1-\lambda} \quad (5)$$

根据三角形的两边之差小于第三边,则有

$$S = \sqrt{(L+R)^2 - e^2} - \sqrt{(L-R)^2 - e^2}$$

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$$= R \left[\sqrt{\left(\frac{L}{R} + 1\right)^2 - 2} - \sqrt{\left(\frac{L}{R} - 1\right)^2 - 2} \right] > 2R \quad (6)$$

排出冲程的平均速度为

$$v_{排} = \frac{S}{t_1} = \frac{S}{1} = \frac{S}{+} \quad (7)$$

吸入冲程的平均速度 $v_{吸}$

$$v_{吸} = \frac{S}{t_2} = \frac{S}{2} = \frac{S}{-} \quad (8)$$

令 $\lambda = \frac{L}{5}, \frac{1}{4}$, $\lambda = 0 \sim 0.4$, 根据式 (1) ~ (8), 计算冲程和柱塞平均速度, 见表 1。

表 1 不同 λ 值时冲程、柱塞平均速度对比

	S/m	$v_{排}/(m \cdot s^{-1})$	$v_{吸}/(m \cdot s^{-1})$	备注
$\frac{1}{5}$	0	2R	0.636 6R	对心式
	0.2	2.001 7R	0.633 8R	正偏置
	0.4	2.006 7R	0.632 0R	正偏置
$\frac{1}{4}$	0	2R	0.636 6R	对心式
	0.2	2.002 7R	0.632 1R	正偏置
	0.4	2.010 8R	0.629 3R	正偏置

从表 1 可以看出, 采用正偏置结构与采用对心式结构相比, 可以增加冲程长度, 但增加量很小, 每增加 0.1, 冲程 S 增加 0.1% ~ 0.2%, λ 值越大, 增加量越大; 排出冲程时柱塞速度有所降低, 每增加 0.1, $v_{排}$ 降低 0.1% ~ 0.2%, λ 值越大, 降低量越大; 吸入冲程时柱塞速度有所增加, 每增加 0.1, $v_{吸}$ 增加 0.3% ~ 0.6%, λ 值越大, 增加量越大。可见, 偏置对于冲程长度及柱塞的速度有一定的影响, 但影响量很小, 随着 λ 值的增加, 影响量逐渐增大。

下面讨论正偏置结构对于连杆传力性能的影响。如图 1 所示, 曲柄 OA 通过连杆 AB 将力 P 传给十字头, 力 P 可以分解为沿十字头速度方向的力 P_t 和与十字头导板垂直的力 P_n , 其中 P_t 是推动十字头运动的有效分力, 而 P_n 只能使十字头和导板间正压力和摩擦阻力增大。则有

$$P_t = P \cos \alpha \quad (9)$$

$$P_n = P \sin \alpha \quad (10)$$

上两式中 α 是力 P 与十字头速度方向的夹角, 可以称之为压力角。从上两式可以看出, $|\alpha|$ 越小, 则有效分力 P_t 愈大, P_n 愈小, 连杆力 P 利用得越充分。从图 1 可以看出正偏置与对心式相比, $|\alpha|$ 的最大值和平均值均减小了, 所以可以得出正偏置提高了连杆的传力性能的结论。

$$\sin \alpha = \frac{-R \sin \theta - e}{L} = - \sin \theta \quad (11)$$

$$P_n = P \sin \alpha = P(- \sin \theta)$$

$$= P(- \sin \theta) \quad (12)$$

连杆传递推力主要在排出冲程, 而排出冲程时 $\sin \theta$ 基本为负值, 其值在 $(-1 \sim 0)$ 之间, 从式 (11) 可得出 λ 取 0.5 时, $|\sin \alpha|$ 的最大值达到最小, 为 0.5, 所以从理论上讲, λ 取值接近 0.5 时比较合理, 但偏置过多对泵的结构设计不利, 实际设计中一般取 $\lambda < 0.5$ 。从式 (12) 可以得出对 P_n 的影响较大, 现取一特殊的曲柄转角 $\theta = -\frac{\pi}{2}$ 来讨论 λ 对 P_n 的影响程度, 此时 P_n 为最大值, 表示为 P_{nmax} , 则 λ 对 P_{nmax} 的影响见表 2。

表 2 λ 对 P_{nmax} 的影响

	0	0.1	0.2	0.3	0.4
P_{nmax}/N	P	$0.9P$	$0.8P$	$0.7P$	$0.6P$

从表 2 可以得出, λ 每增加 0.1, P_{nmax} 减少 10%。正偏置的这一特点可以有效地减少十字头和导板间的摩擦, 从而改善其偏磨的情况 (同时, 摩擦阻力的减少可以提高整个泵的效率), 尤其是 P 值比较大时, 这种效果更加明显。所以在一些压力高或者由于结构的限制选定的 λ 值比较大的情况下, 可以采用正偏置设计来改善十字头与导板间的正压力和偏磨。

偏置结构的应用

由于偏置增加了加工和装配的难度, 所以在泵压不是很高, λ 值不是很大时, 一般不采用偏置结构。目前, 国内外生产的油田用泵中, 绝大多数采用对心式设计, 有少数结构紧凑、泵压较高的泵采用了正偏置设计, 例如 SPM TWS600S 型柱塞泵, 该泵体积较小, 泵压较高, 采用正偏置结构比较合理。该泵偏置距 e 为 19.05 mm, 偏置比 λ 为 0.25。SPM TWS600S 泵在油田使用效果很好, 广泛应用于压裂、固井作业。该泵结构紧凑, 质量轻, 特别方便移运和车上布置。正偏置结构减小了十字头对导板的正压力和摩擦力, 延长了十字头和导板的寿命。同时, 由于其性能可靠, 零部件返修率低, 深受用户欢迎。

对于反偏置结构, 不但减弱了连杆的传力性能, 而且增加了十字头和导板间的正压力和摩擦阻力, 所以一般不予采用。

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bined loads of torsion force , bending moment , torsion moment and internal pressure is derived. In addition , the methods for the solution of L^r parameter are presented.

Key words : combined load , limit load , cracked pipeline , L^r parameter , graphic method

Li Rong (57 Petroleum Machinery Co. , Ltd. , Jingzhou City , Hubei Province) , Yang Xiaoli , Wang Bo , et al. Kinematic and dynamic analysis of reciprocating offset slidercrank mechanism. CPM , 2004 , 32 (11) : 18 ~ 19

In order to make clear the performance characteristics of offset structure and improve the design of reciprocating pumps , kinematic and dynamic analysis of offset slidercrank mechanism is made. The influence of the offset structure on stroke length , plunger suction and discharge rate and force transfer capacity of the connecting rod as well as the effect of crosshead on positive pressure of guide plate are analyzed. It is indicated that the force transfer capacity of the connecting rod can be improved and the crosshead positive pressure on the guide plate can be reduced by adopting the positive offset structure.

Key words : reciprocating pump , offset , slidercrank mechanism , kinematic analysis

Zhang Qiang (Carbon Fiber Research Center of Shandong University , Jinan) , Zhu Bo , Cai Huasu. Investigation in the characteristics of carbon fiber continuous sucker rod with phenolic resin as matrix. CPM , 2004 , 32(11) : 22 ~ 24

Since the conventional carbon fiber continuous sucker rod has low corrosion resistance in deep holes , a carbon fiber sucker rod taking modified phenolic resin as matrix is developed. Compared with the carbon fiber rod using epoxy resins or vinyl ester resin as matrix , the carbon fiber rod with phenolic resin as matrix has better mechanical properties and higher heat - and corrosion resistance , and is more suitable for use in the production of deep holes.

Key words : phenolic resin , carbon fiber continuous sucker rod , characteristics , investigation

Ma Dingfu (Shifang Huifeng Oil Production Equipment Company , Shifang City , Sichuan Province) , Qian Yicheng , Yang Xiaoping. Safety control system for high - pressure antisulphur wellhead. CPM , 2004 , 32(11) : 28 ~ 29

To ensure safety of the well site , a safety control system for high - pressure antisulphur wellhead is developed. The system is mainly comprised of gas source

filtering and regulating unit , electronic monitoring meter , pneumatic control unit , pneumatic sensing unit and pneumatic execution unit. By means of this system , the wellhead can be shut down in 3 - 4 seconds in case of emergency. The operating process and field use of the system is introduced.

Key words : high pressure sour gas well , oil and gas wellhead , safety control system

Lu Shilin (Jinzhou Oil Production Plant , Liaohe Oilfield Company , Linghai City , Liaoning Province) , Liang Shoucai , Wang Zhiming , et al. Development and application of forced - closing - and - opening plunger pump. CPM , 2004 , 32(11) : 30 ~ 31

A forced - closing - and - opening plunger pump is developed to solve the problems of gas lock and sand inflow and low pump efficiency in steam injection wells. The travelling valve of the pump is designed to be closed and opened forcibly , and the pump plunger adopts equal - diameter bare pipe with a floating structure to prevent gas lock and sand sticking. The pump was used in Jinzhou Oil Production Plant , and good effect has been achieved.

Key words : plunger pump , structural design , field use

Zhang Xuemei (Oil Production Technology Research Institute , Shengli Oilfield Company , Dongying City , Shandong Province) , Li Changyou , Chi Peng , et al. Development of Intelligent multiparameter wellhead metering system. CPM , 2004 , 32(11) : 32 ~ 33

In the light of the problems with metering of data of formation testing in Shengli Oilfield , an intelligent multiparameter wellhead metering system for single hole is developed. The system is made up of testing module , data acquisition module and gas separation module. It can carry out continuous metering of produced fluid automatically. Skid - mounted , it can be moved and installed conveniently , therefore can meet the need of testing and metering of viscous oil wells and remote wells.

Key words : metering equipment , intelligent metering , multiparameter , skid - mounted , continuous metering

Cong Wansheng (Baoji Oilfield Machinery Co. , Ltd. , Baoji City , Shaanxi Province) , Zheng Mingjian , Yang Xiangqian. IPC - PLC - PROFIBUS - based intelligent control system for electrical drive drilling rigs. CPM , 2004 , 32(11) : 36 ~ 40

Th application of IPC - PLC - PROFIBUS - based intelligent control system on 7000 m AC variable - fre-